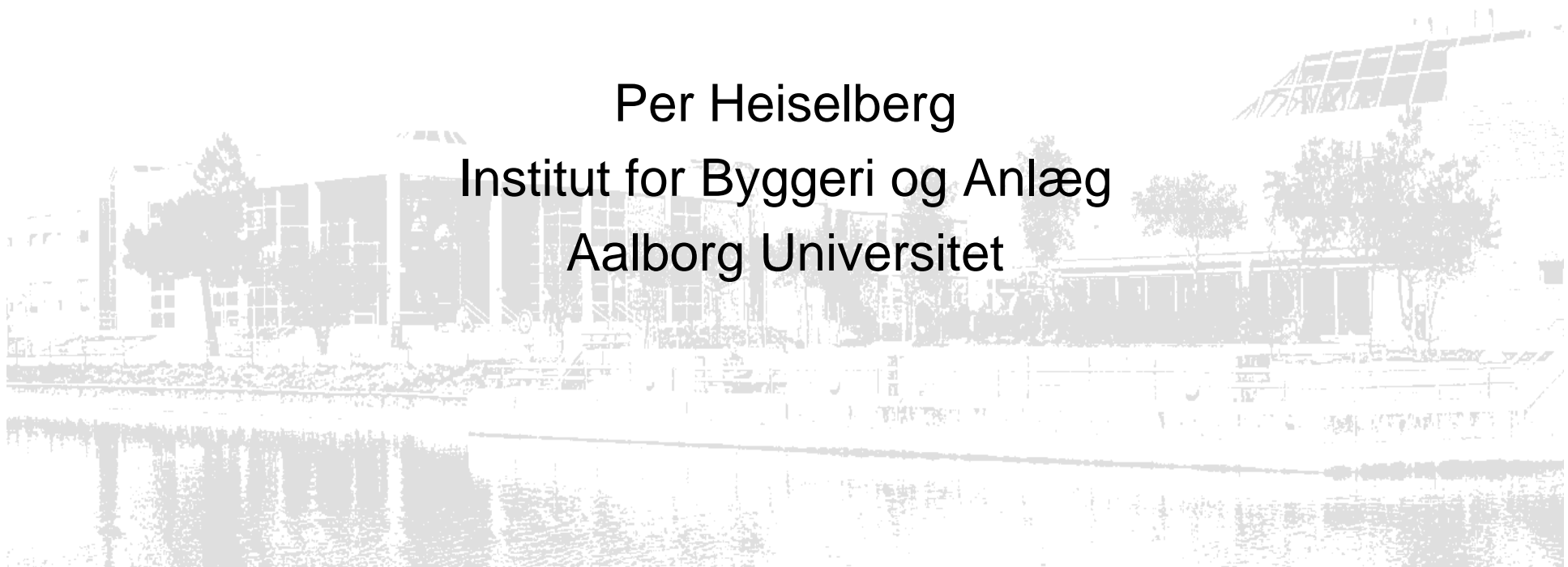


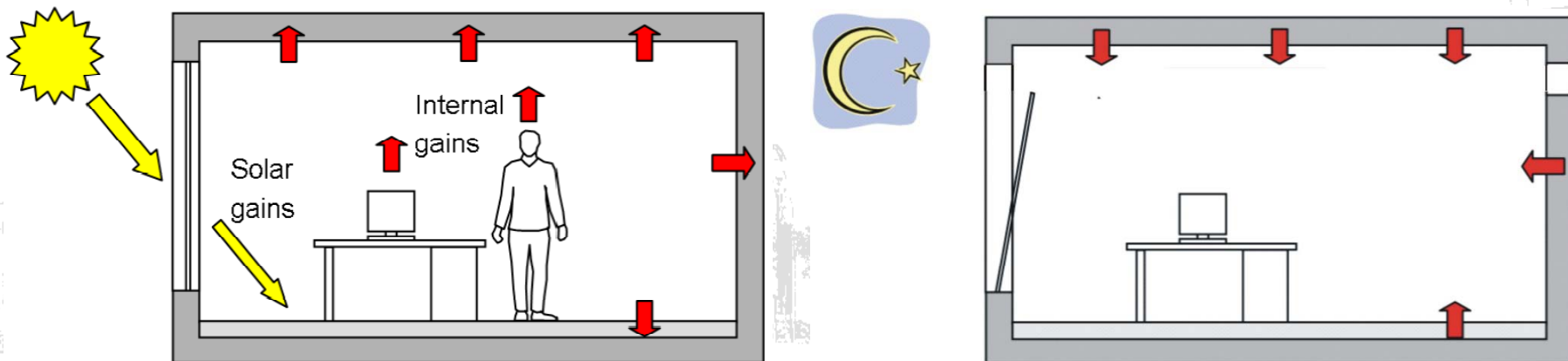
Udnyttelse af betons termiske egenskaber til forbedret indeklima og reduceret energiforbrug

Per Heiselberg
Institut for Byggeri og Anlæg
Aalborg Universitet



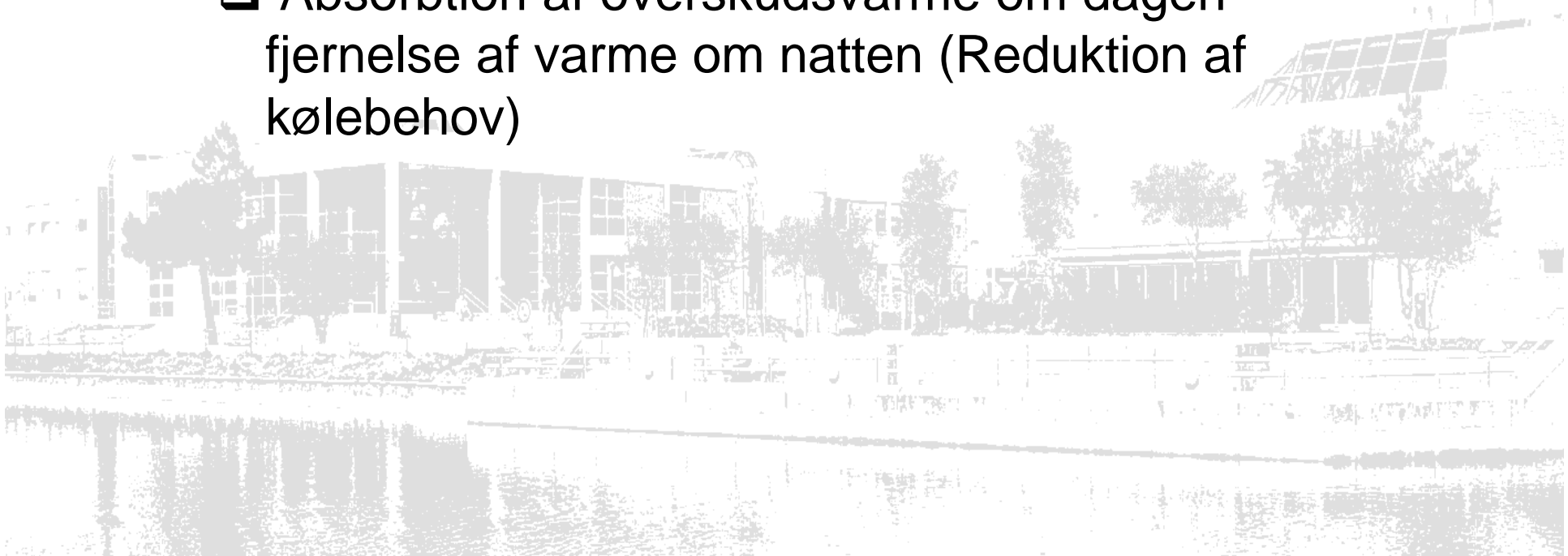
Energi akkumulering – Hvad er den basale funktion?

- ❑ Varmemodulering (24 timers cyklus)
 - ❑ Absorbtion af overskudsvarme om dagen – tilbagelevering af varme om natten (reduktion af varmebehov)



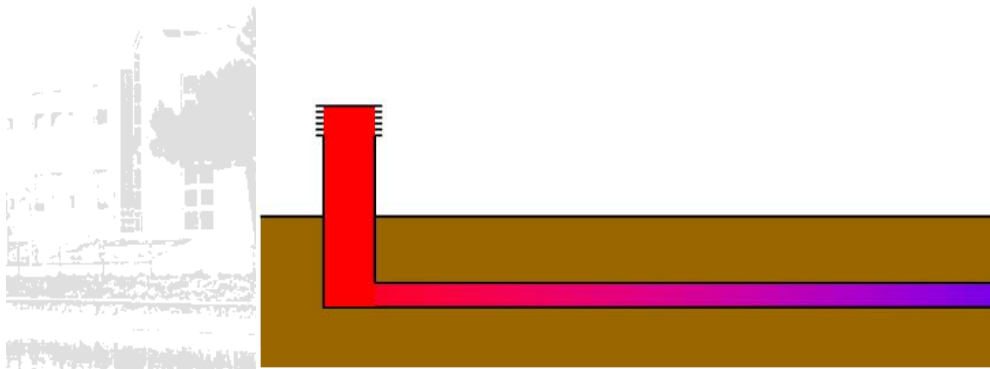
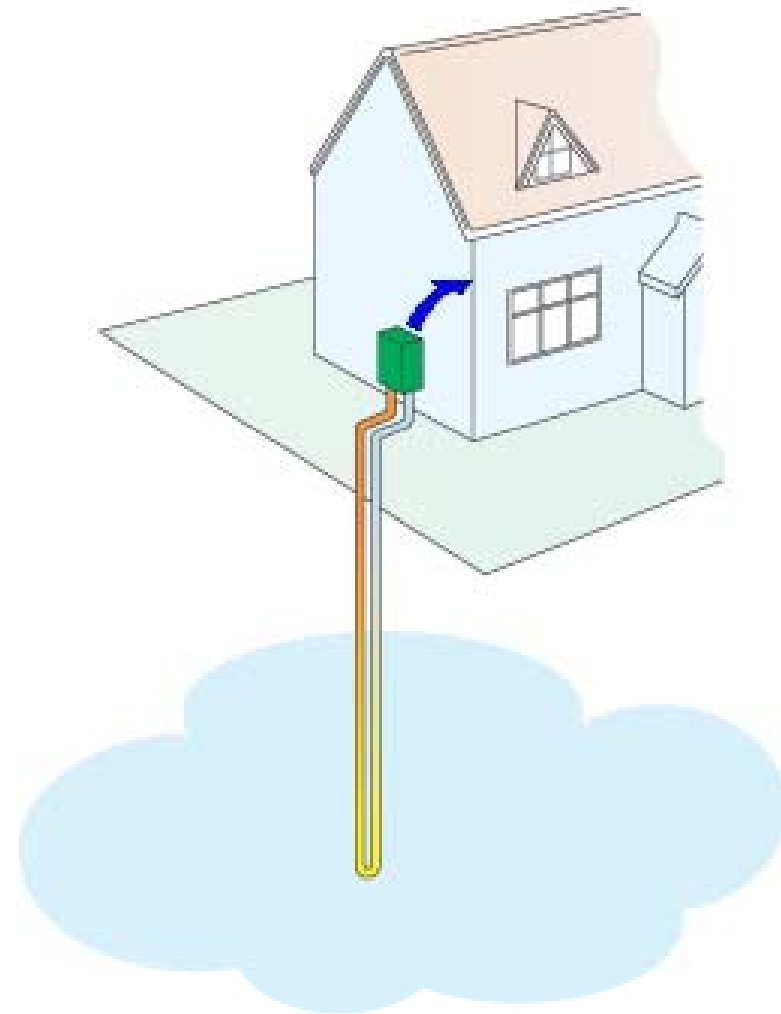
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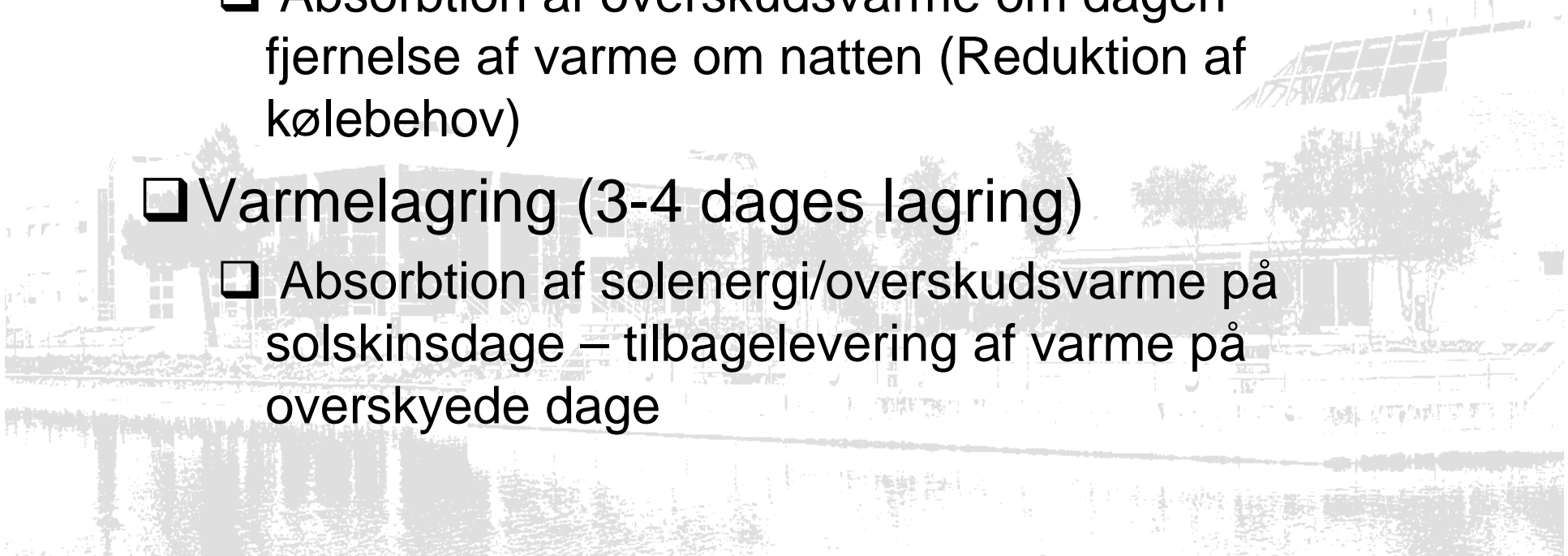
Natural heat sinks

- Night-time outdoor air
- Earth-to-air (water) heat exchanger
- Ground water

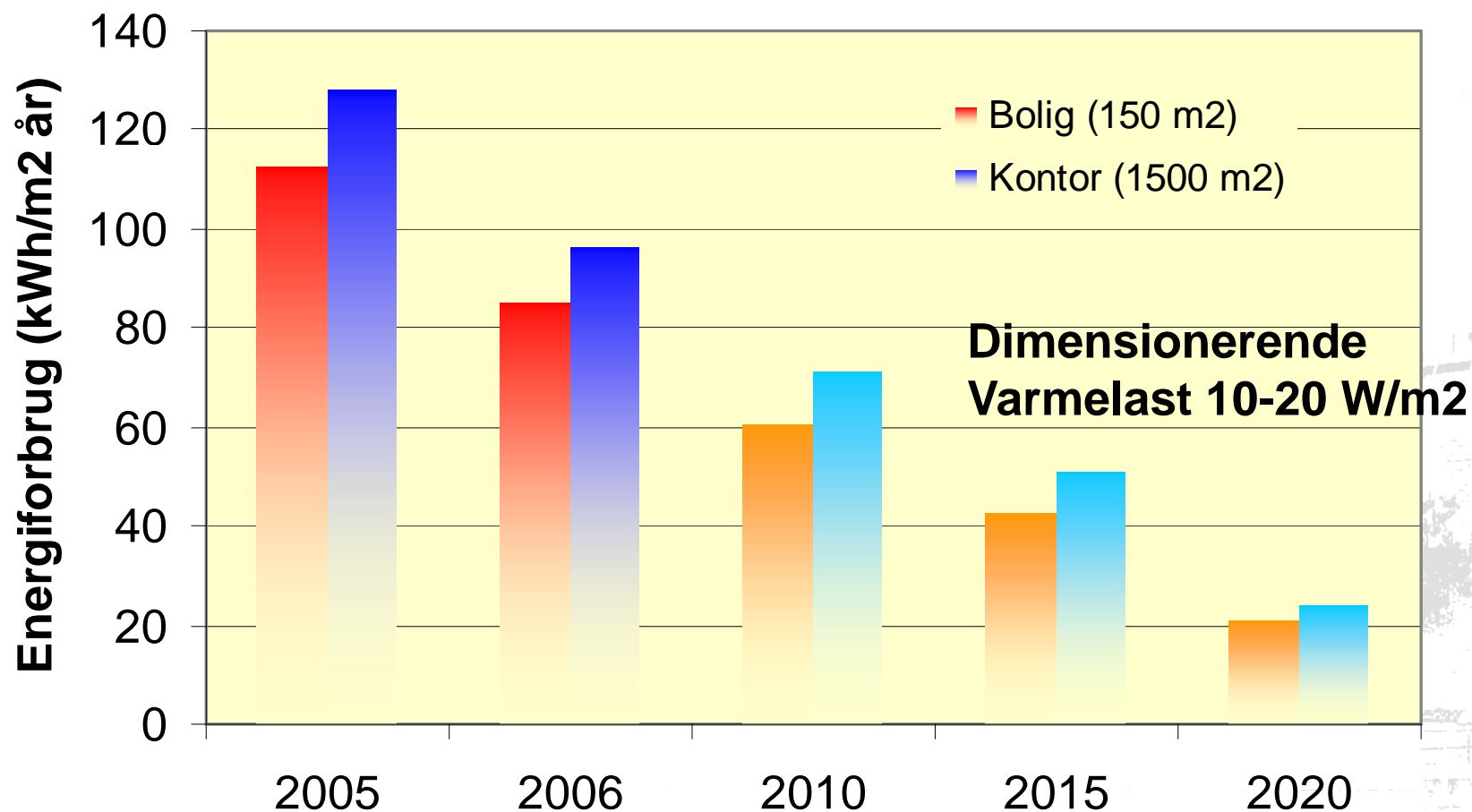


Energi akkumulering – Hvad er den basale funktion?

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 - Absorbtion af overskudsvarme om dagen – fjernelse af varme om natten (Reduktion af kølebehov)
- Varmelagring (3-4 dages lagring)
 - Absorbtion af solenergi/overskudsvarme på solskinsdage – tilbagelevering af varme på overskyede dage

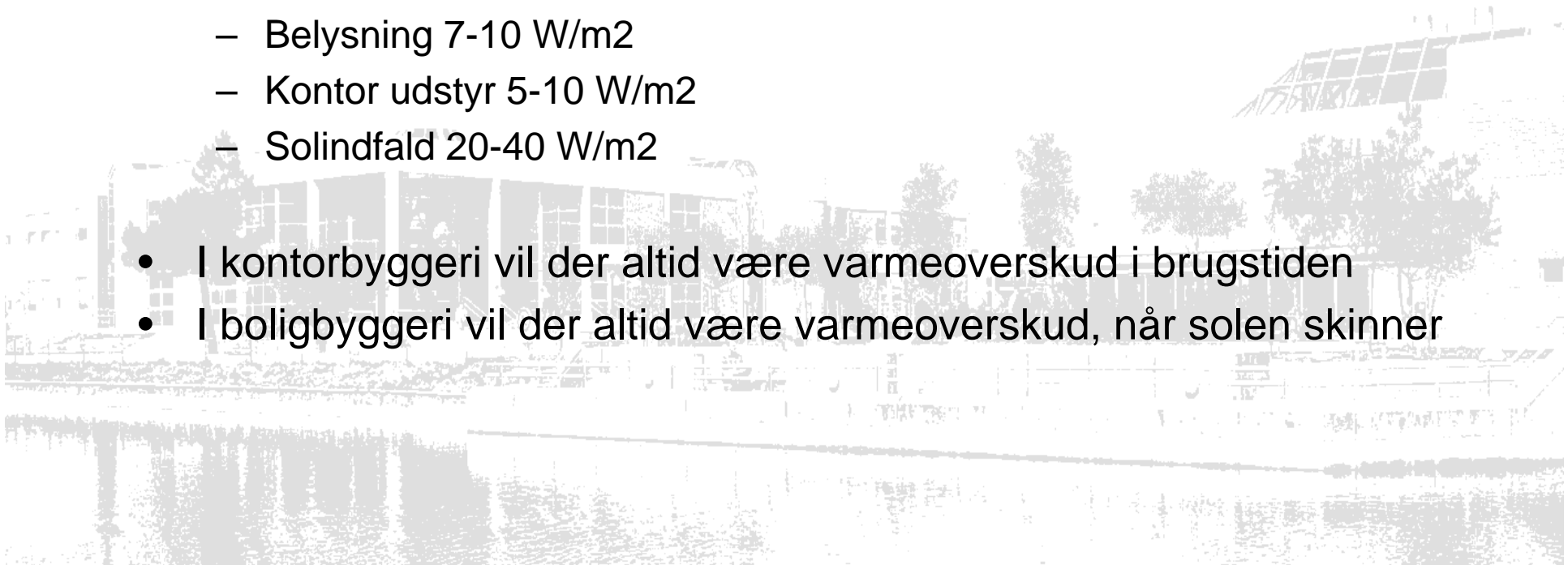


Udvikling i maksimalt energiforbrug i nye bygninger



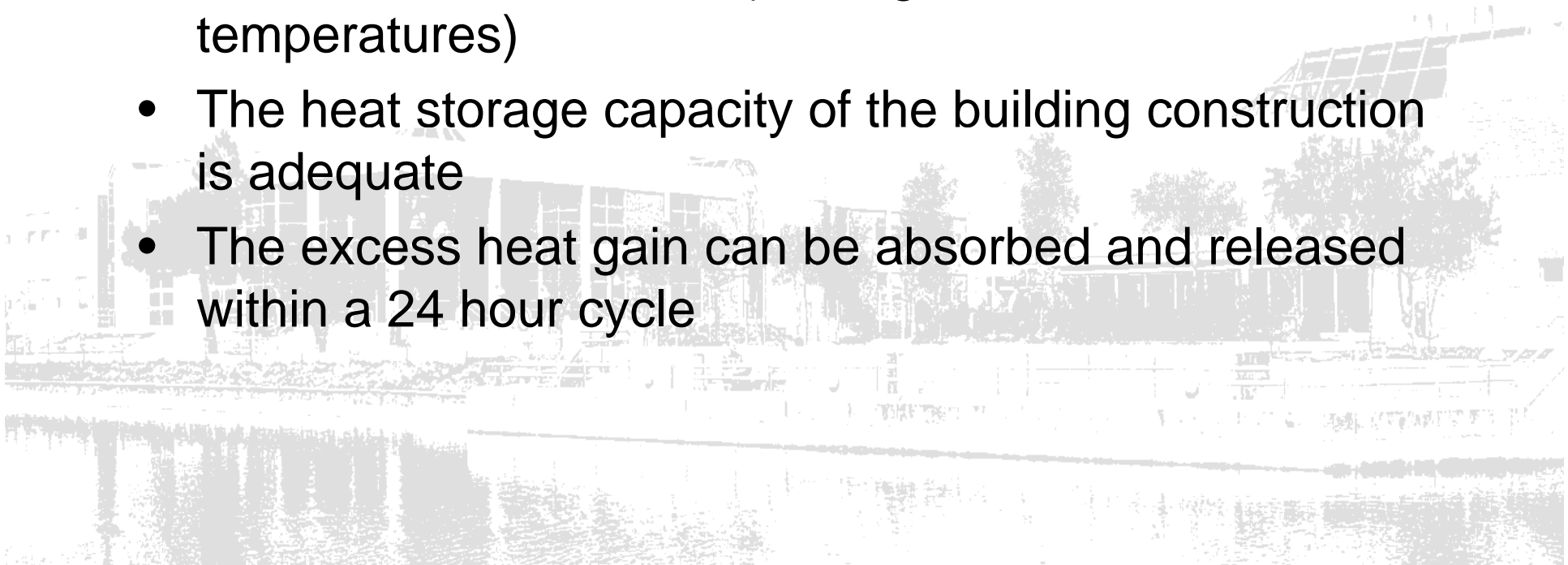
Varmebehov/varmetilskud

- Varmebehov
 - Dimensionerende 10-20 W/m²
 - Gennemsnitlig i vintermånederne 6-12 W/m²
- Varmetilskud
 - Personer 100 W (kontor 5 W/m²)
 - Belysning 7-10 W/m²
 - Kontor udstyr 5-10 W/m²
 - Solindfald 20-40 W/m²
- I kontorbyggeri vil der altid være varmeoverskud i brugstiden
- I boligbyggeri vil der altid være varmeoverskud, når solen skinner



Necessary Conditions for Success

- **It can make a difference** (replacement of heating system and/or air conditioning)
- A heat sink is available (low night-time outdoor air temperatures)
- The heat storage capacity of the building construction is adequate
- The excess heat gain can be absorbed and released within a 24 hour cycle

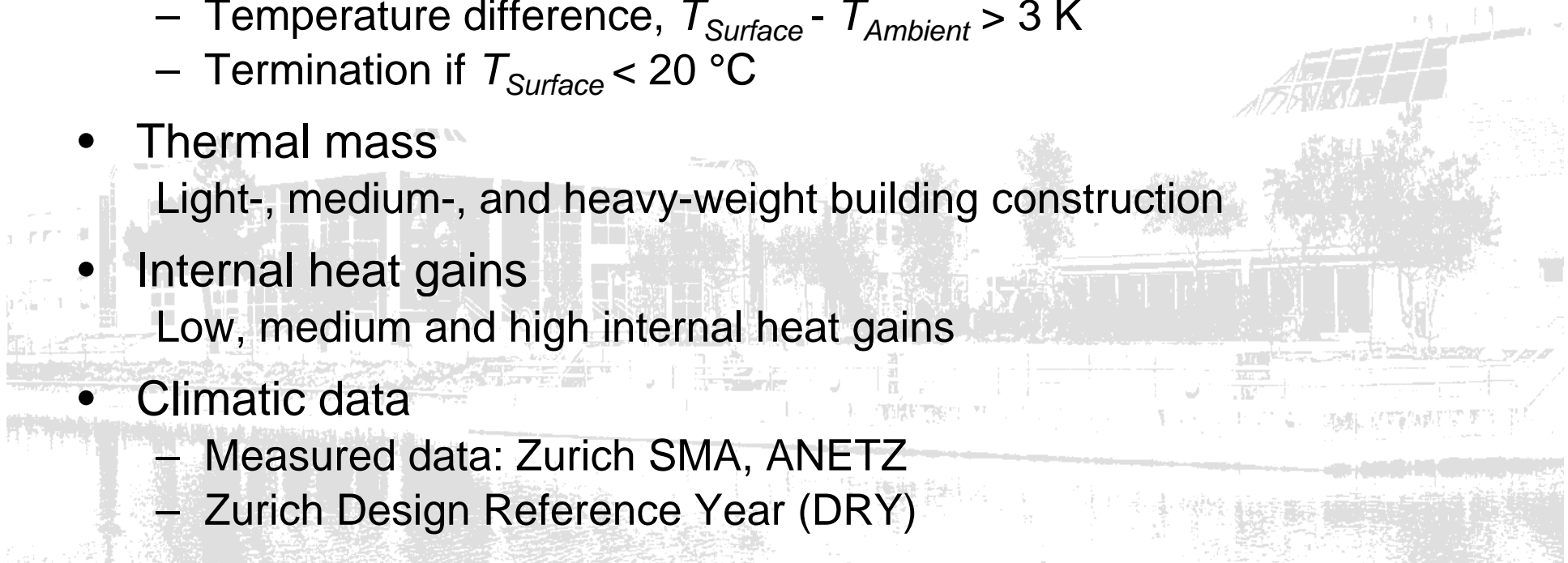
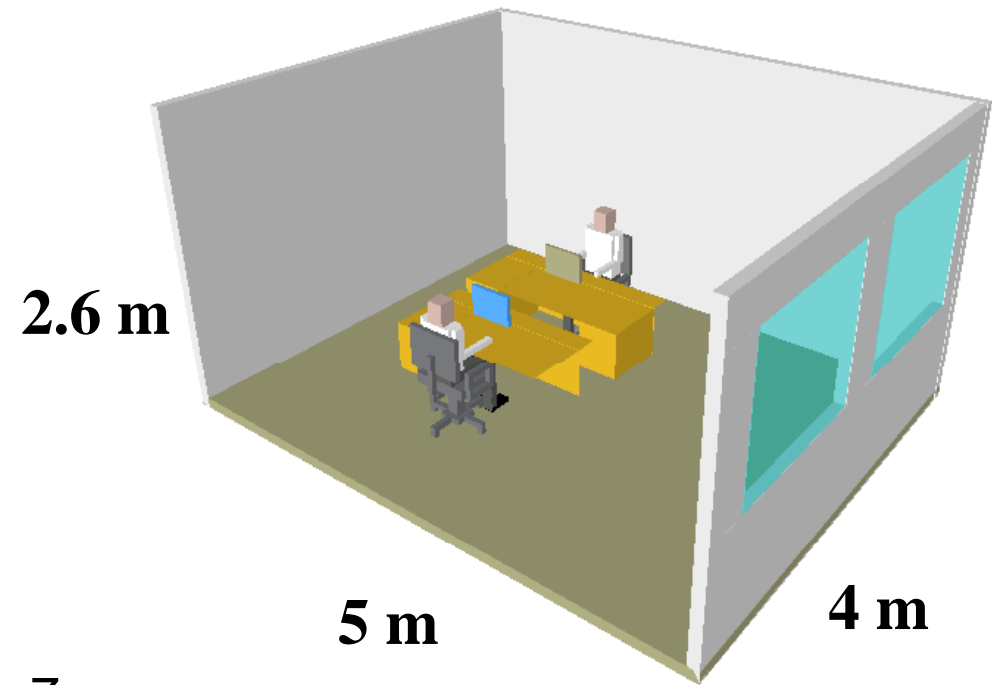


Parameter Study

Office room

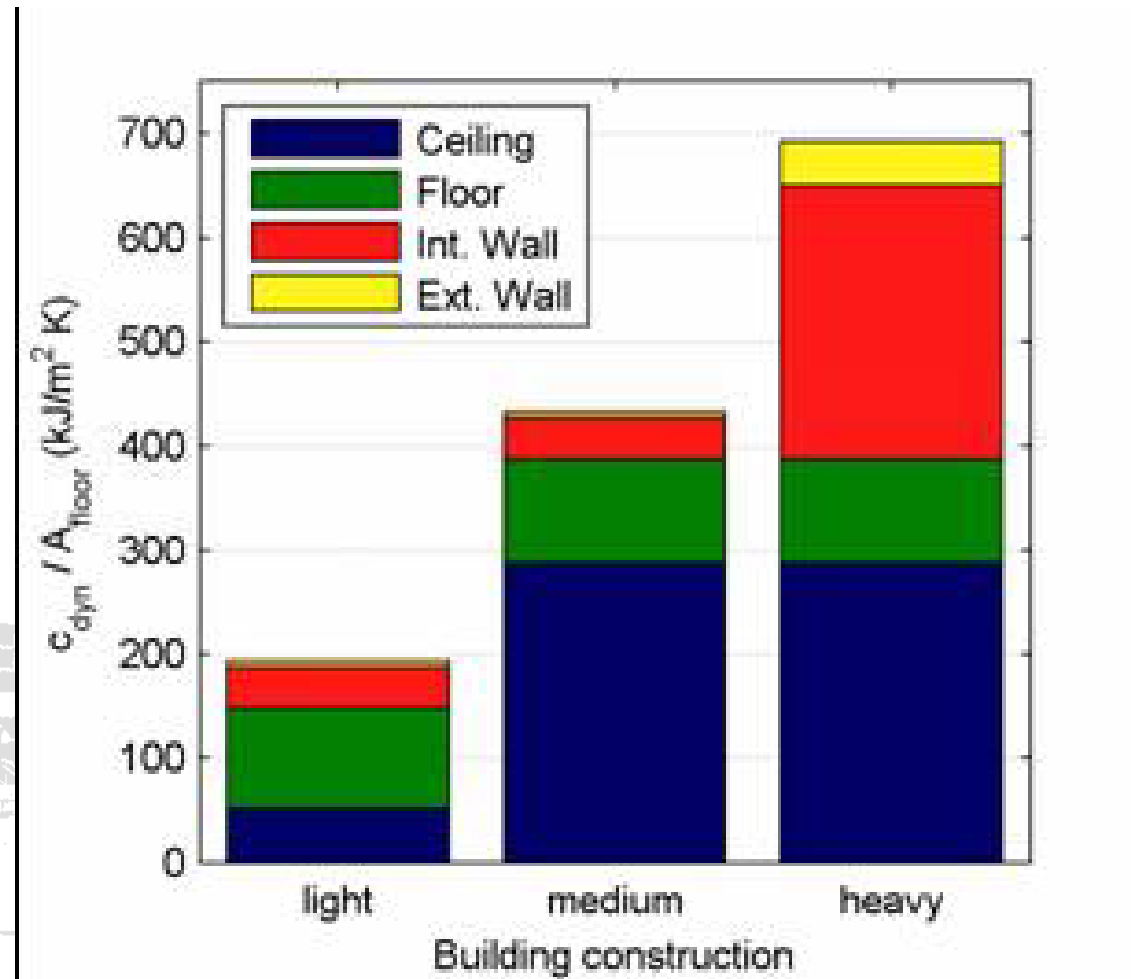
Model in HELIOS

- Night-time ventilation
 - Air change rate: 6 ACH
 - Night ventilation from 7 pm to 7 am
 - Temperature difference, $T_{Surface} - T_{Ambient} > 3 \text{ K}$
 - Termination if $T_{Surface} < 20 \text{ °C}$
- Thermal mass
 - Light-, medium-, and heavy-weight building construction
- Internal heat gains
 - Low, medium and high internal heat gains
- Climatic data
 - Measured data: Zurich SMA, ANETZ
 - Zurich Design Reference Year (DRY)



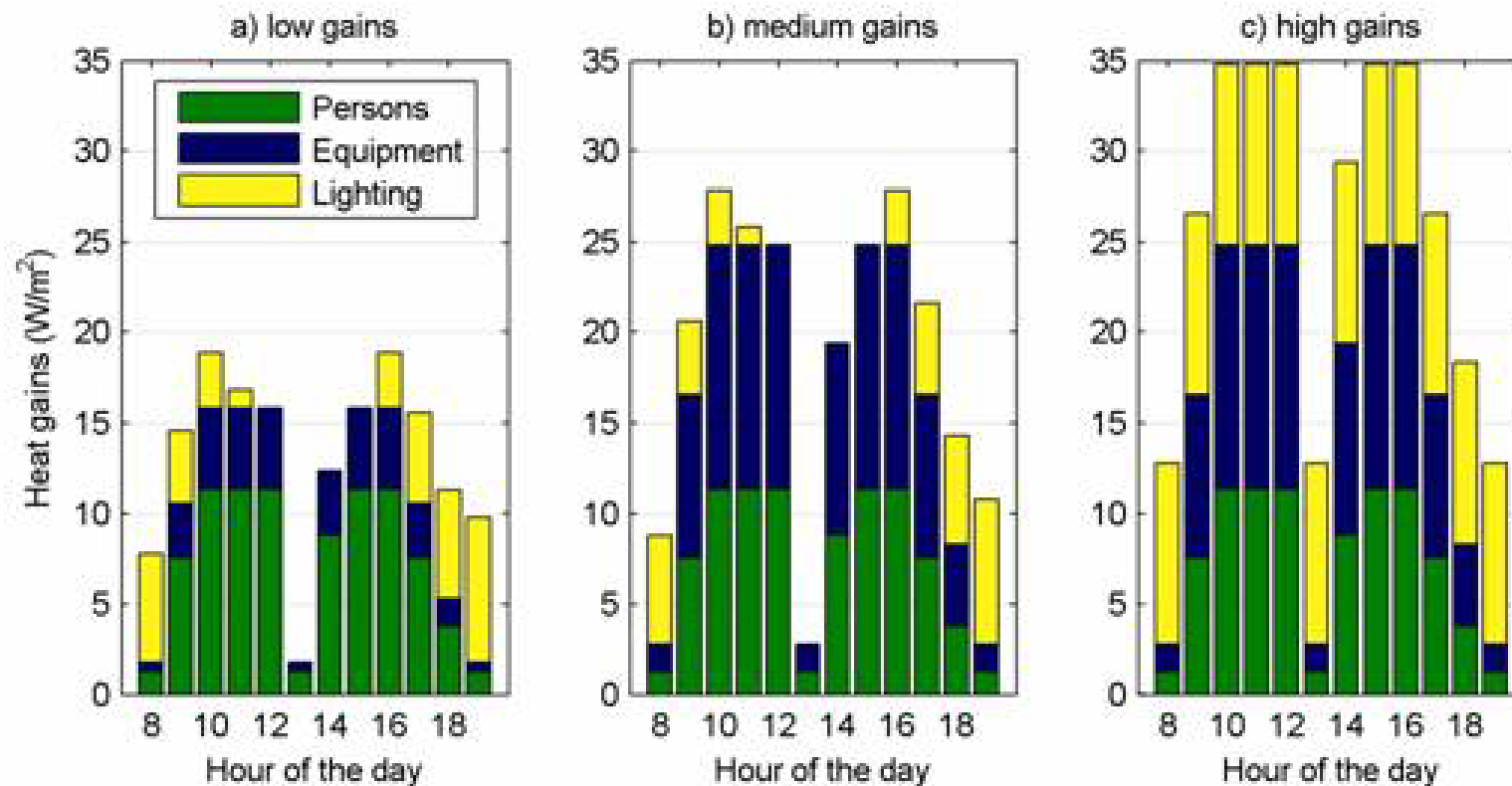
Thermal Mass

- Three different levels of thermal mass
 - light (suspended ceiling, gypsum board walls),
 - medium (exposed concrete ceiling, gypsum board walls)
 - heavy (exposed concrete ceiling, lime sand brick walls)



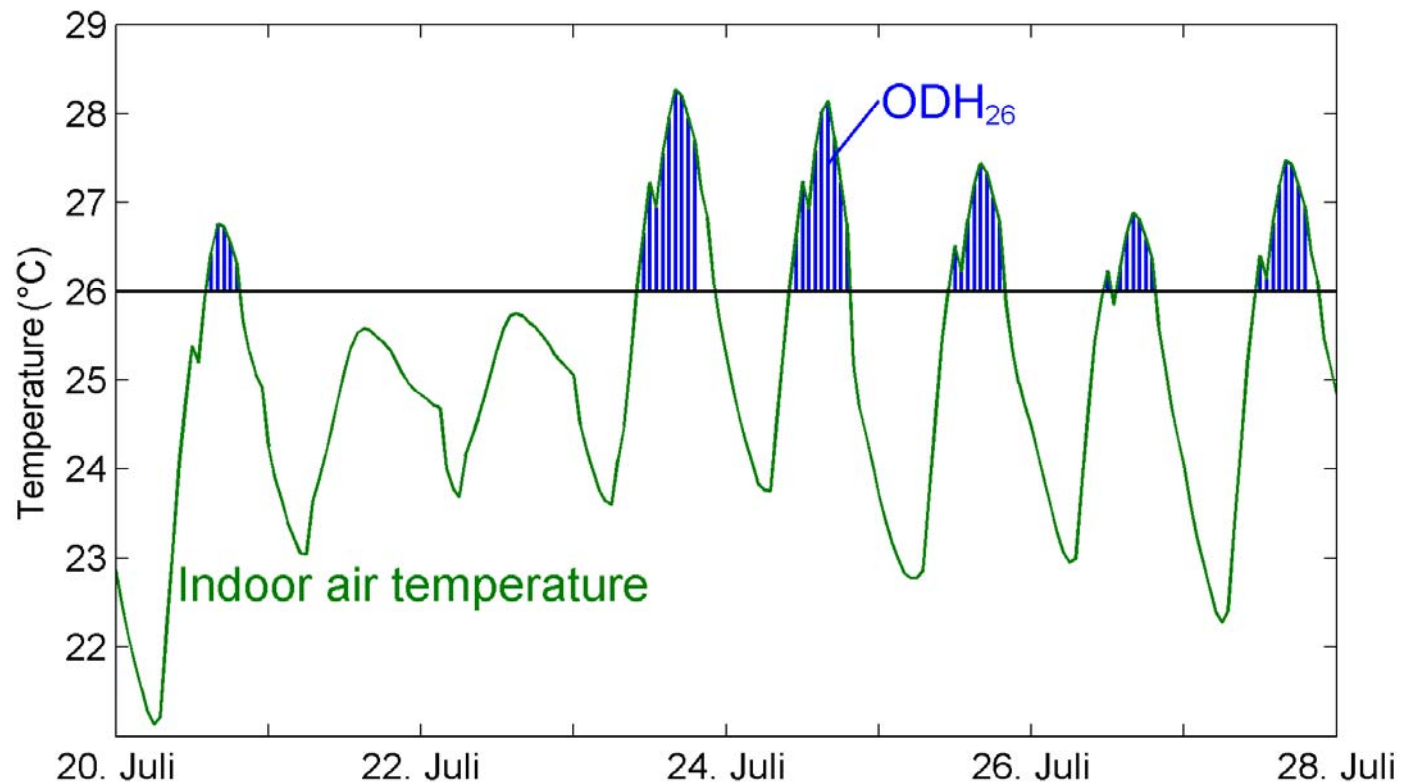
Internal heat gains in the course of a day.

- Low ($159.2 \text{ Wh/m}^2\text{d}$, 13 W/m^2)
- medium ($229.2 \text{ Wh/m}^2\text{d}$, 19 W/m^2)
- high ($313.2 \text{ Wh/m}^2\text{d}$, 26 W/m^2)



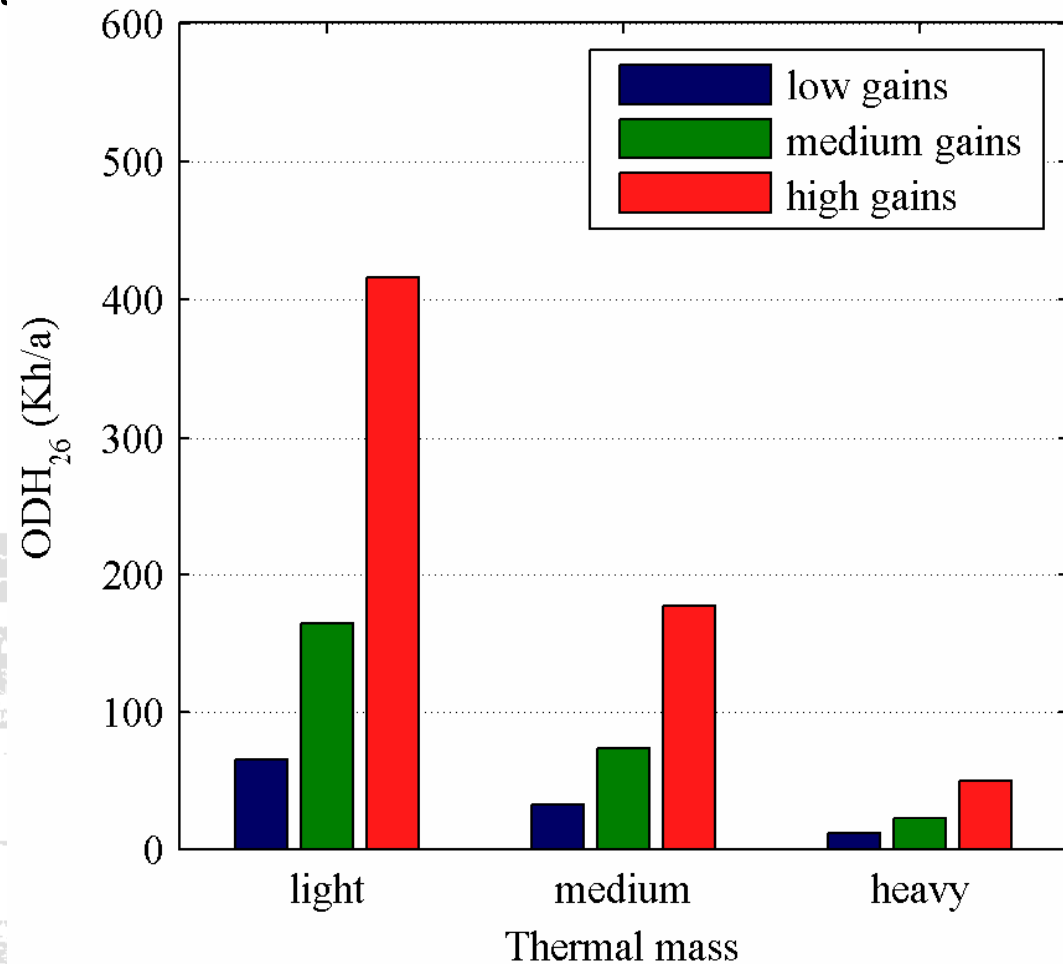
Thermal comfort evaluation

- Overheating degree hours above 26 °C (ODH_{26})
- International standards: $ODH_{26} = 100 - 400$ Kh/a



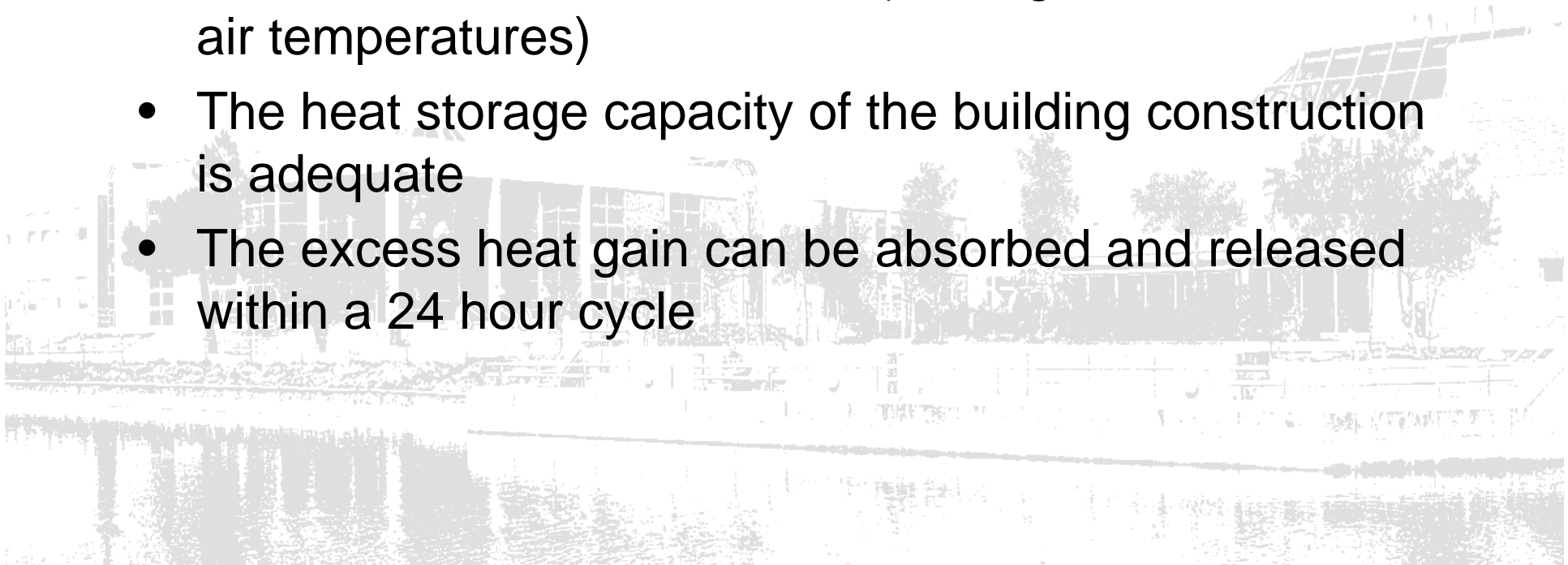
Overheating degree hours above 26 °C

- For Zurich climatic data (ANETZ 1996-2005);



Necessary Conditions for Success

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Climatic potential for night-time cooling

- Degree hours method to quantify the climatic cooling potential (CCP)
- Harmonically oscillating building temperature within a range of thermal comfort:

$$T_b = 24.5^{\circ}\text{C} \pm 2.5^{\circ}\text{C}$$

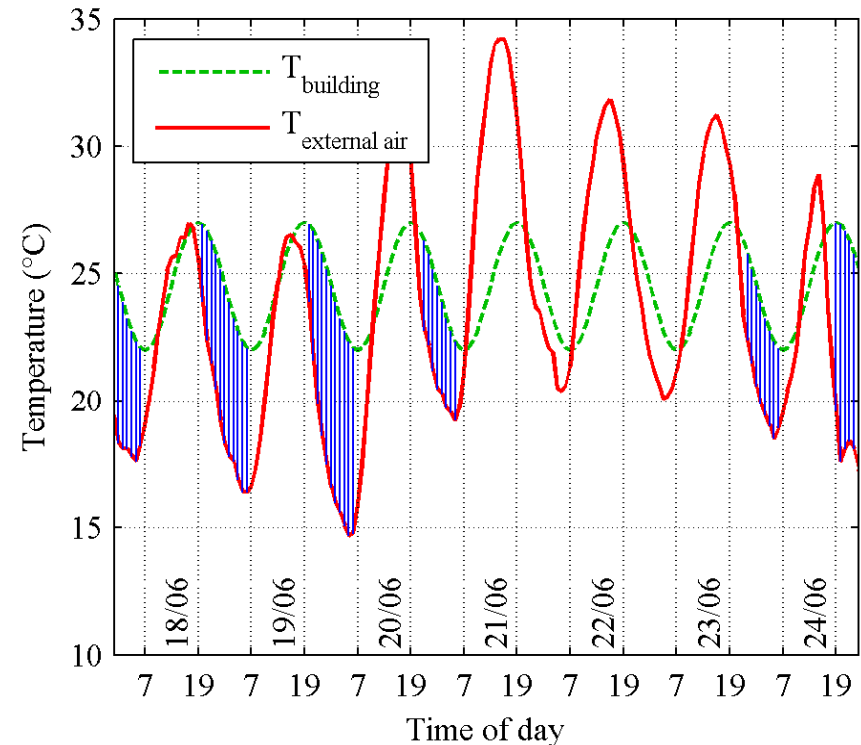
- Ventilation period:
7 pm – 7 am

- Minimum temperature difference: $\Delta T_{crit} = 3\text{K}$

→ $CCP_{t_f}(\text{K h})$

$$CCP_d = \sum_{t=t_i} m_{d,t} (T_{b(d,t)} - T_{e(d,t)})$$

$$\begin{cases} m = 1 \text{ h} & \text{if } T_b - T_e \geq \Delta T_{crit} \\ m = 0 & \text{if } T_b - T_e < \Delta T_{crit} \end{cases}$$

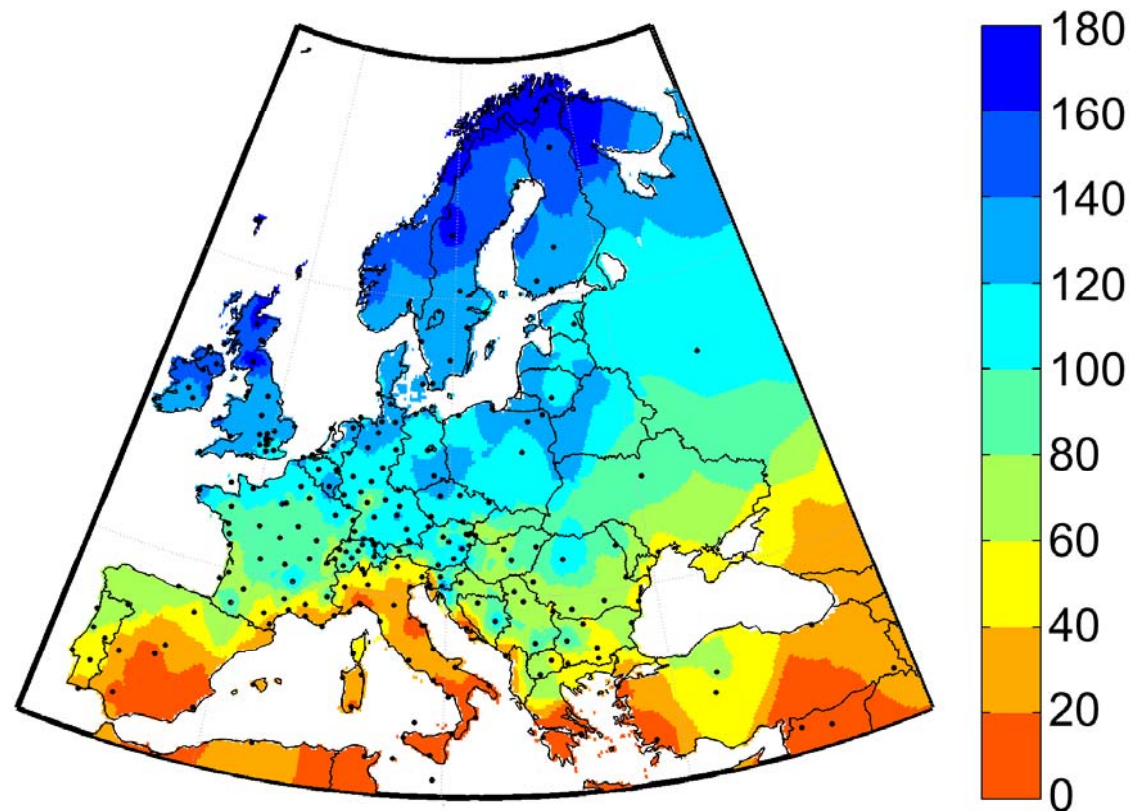


Shaded areas show the climatic cooling potential during one exceptionally hot week in summer 2003 for Zurich SMA (ANETZ data)

Local variability

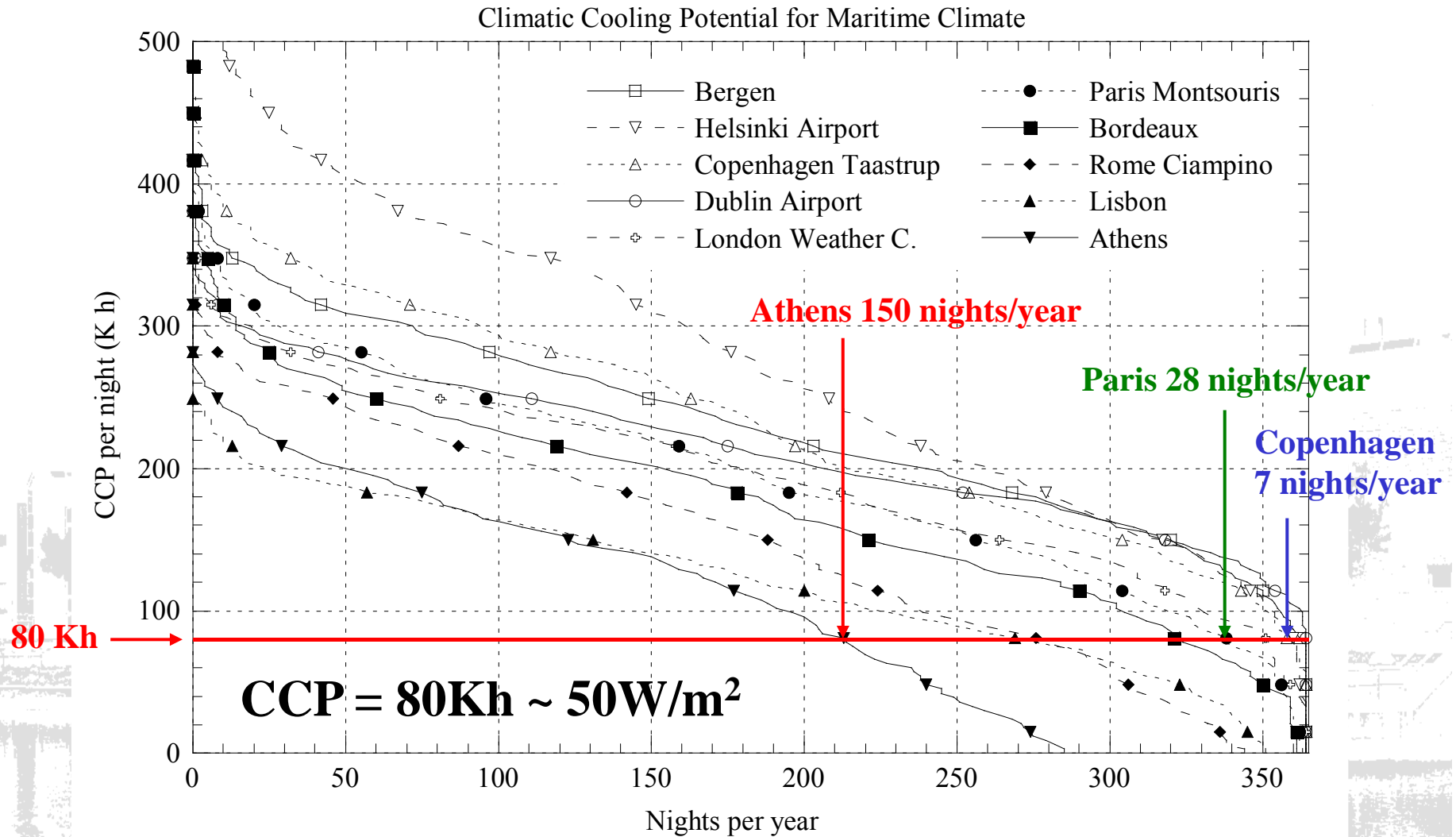
Semi-synthetic data
(Meteonorm) from 259
locations in Europe

- Very high potential of 120 – 180 K h in Northern Europe (incl. British Isles)
- High cooling potential (80 – 140 K h) in Central, Eastern and parts of Southern Europe
- Low cooling potential in Southern Europe: 0 – 80 K h



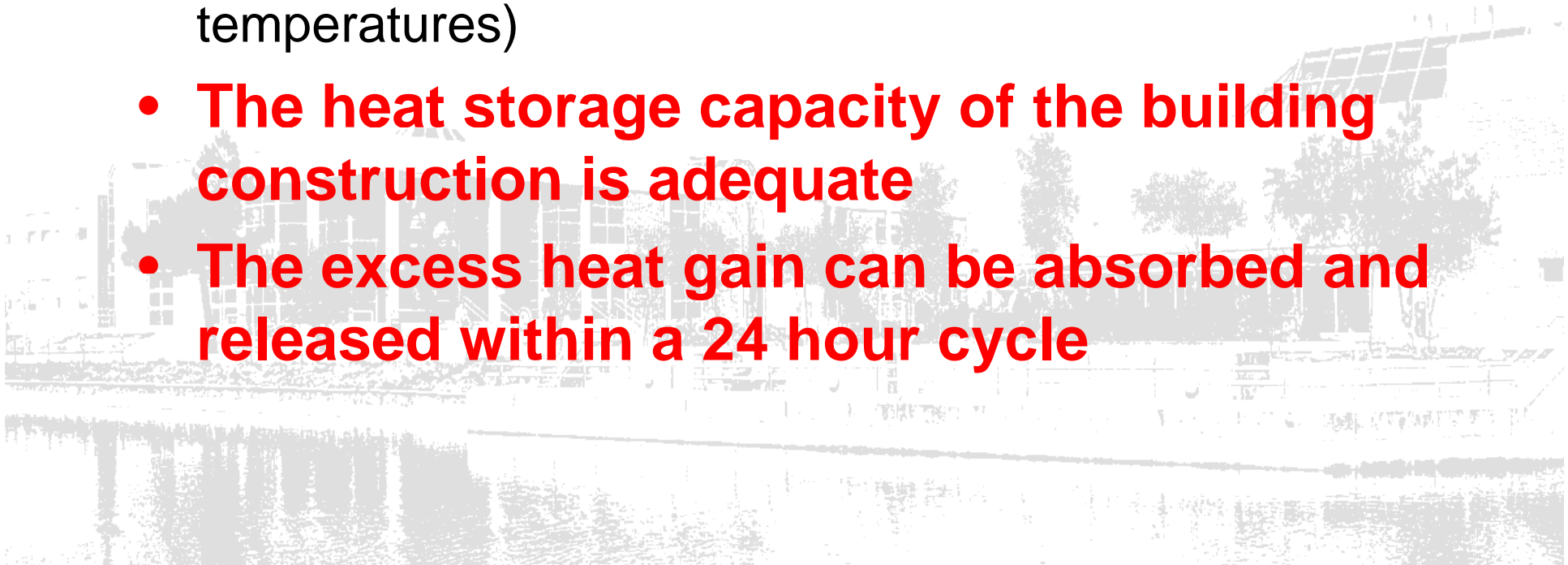
Map of mean climatic cooling potential (K h / night) in July (Meteonorm data)

Cumulative frequency distribution of CCP



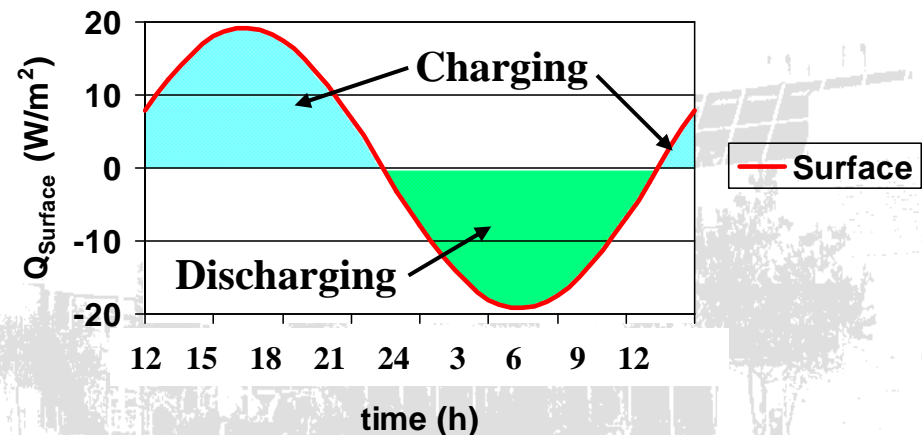
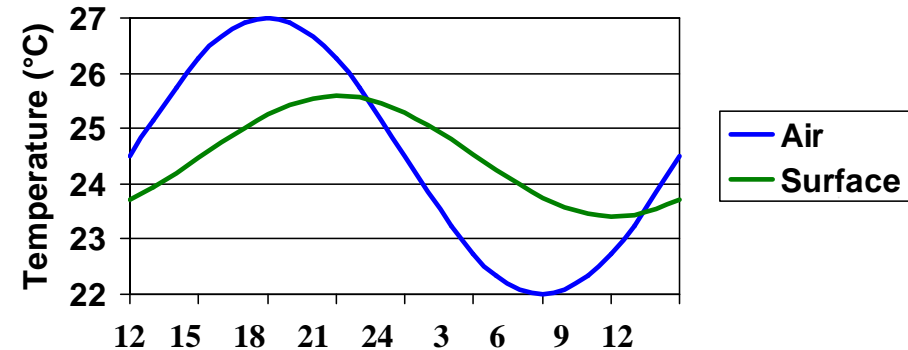
Necessary Conditions for Success

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Dynamic heat storage capacity

- Integration of the charging or discharging surface heat flow over one periodic cycle
- Dynamic heat storage capacity c_{dyn} (kJ/m²K)



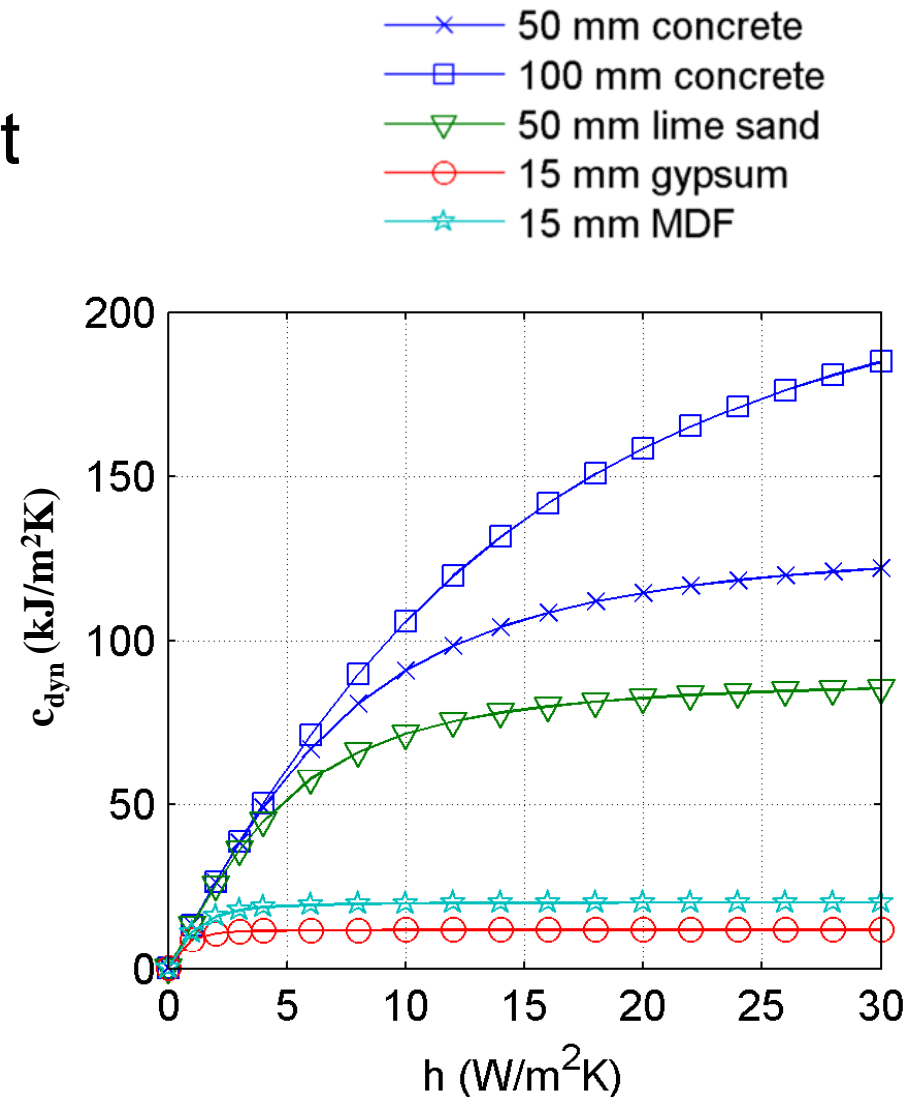
Definition in EN ISO 13786 (1991)
 Thermal performance of building components –
 Dynamic thermal characteristics – Calculation
 methods

Temperature and surface heat flow profiles for
 a 100 mm thick concrete slab, $h = 10$ W/m²K.

Heat transfer coefficient

- Thin slab / light-weight material:
Constant heat storage capacity for $h > 3 \text{ W/m}^2\text{K}$
- Thick slab / heavy-weight material:
Significant increase in heat storage capacity with increasing HTC up to $h = 30 \text{ W/m}^2\text{K}$

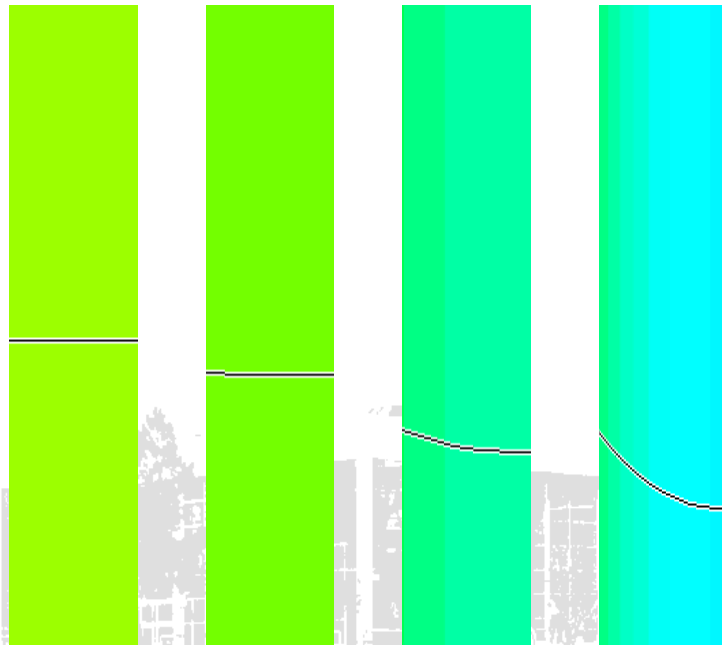
	λ W/mK	ρ kg/m ³	c kJ/kgK
Concrete	1.80	2400	1.1
Lime Sand	1.10	2000	0.9
Gypsum	0.40	1000	0.8
MDF	0.18	800	1.7



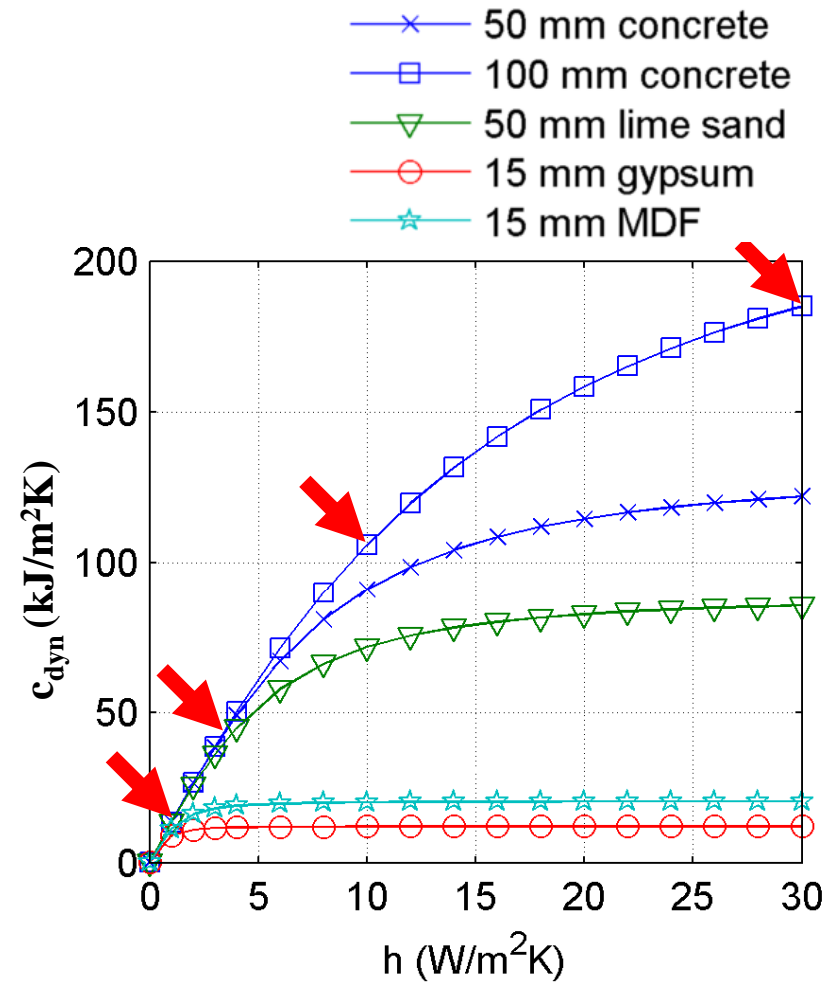
Diurnal heat storage capacity, c_{dyn} depending on the heat transfer coefficient, h for different materials and slab thicknesses.

Heat transfer coefficient

Concrete, $d = 100$ mm



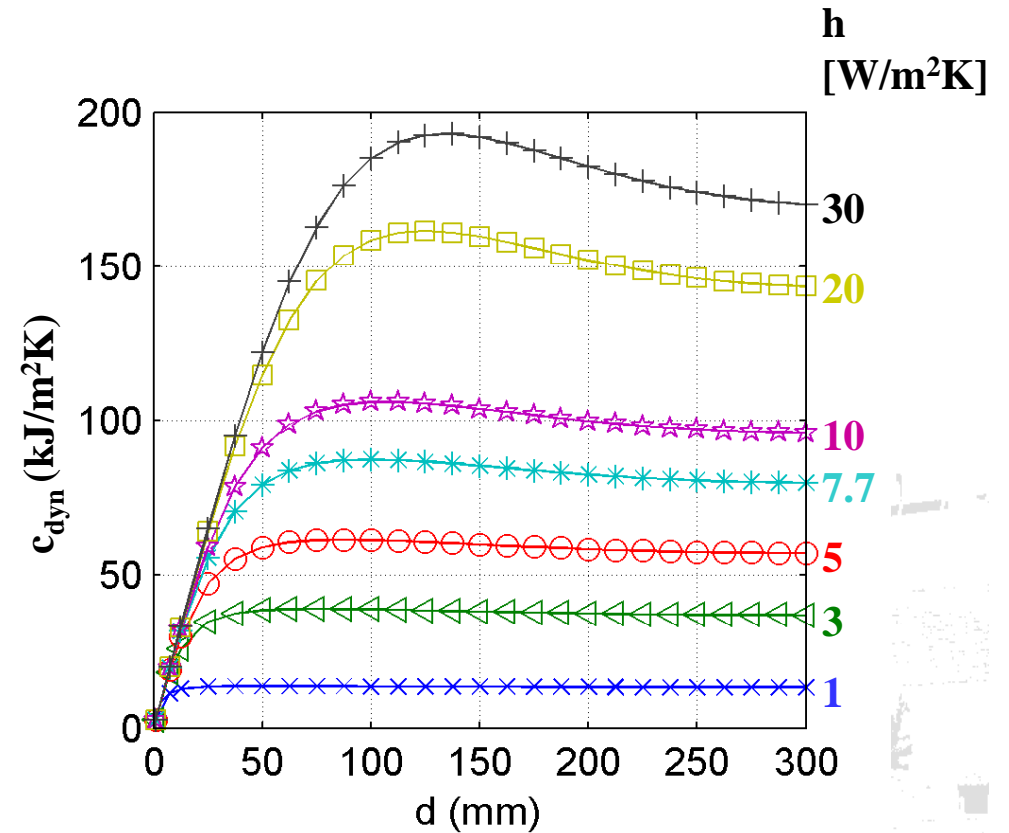
$h = 1 \dots 3 \dots 10 \dots 30$ W/m²K



Diurnal heat storage capacity, c_{dyn} depending on the heat transfer coefficient, h for different materials and slab thicknesses.

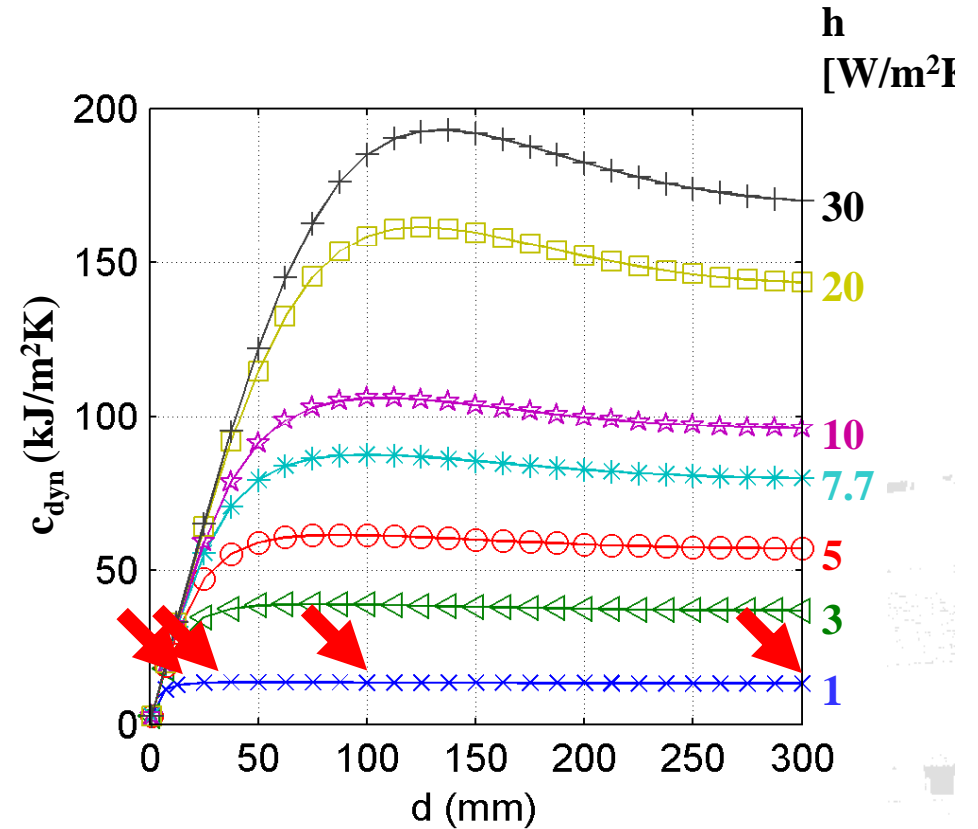
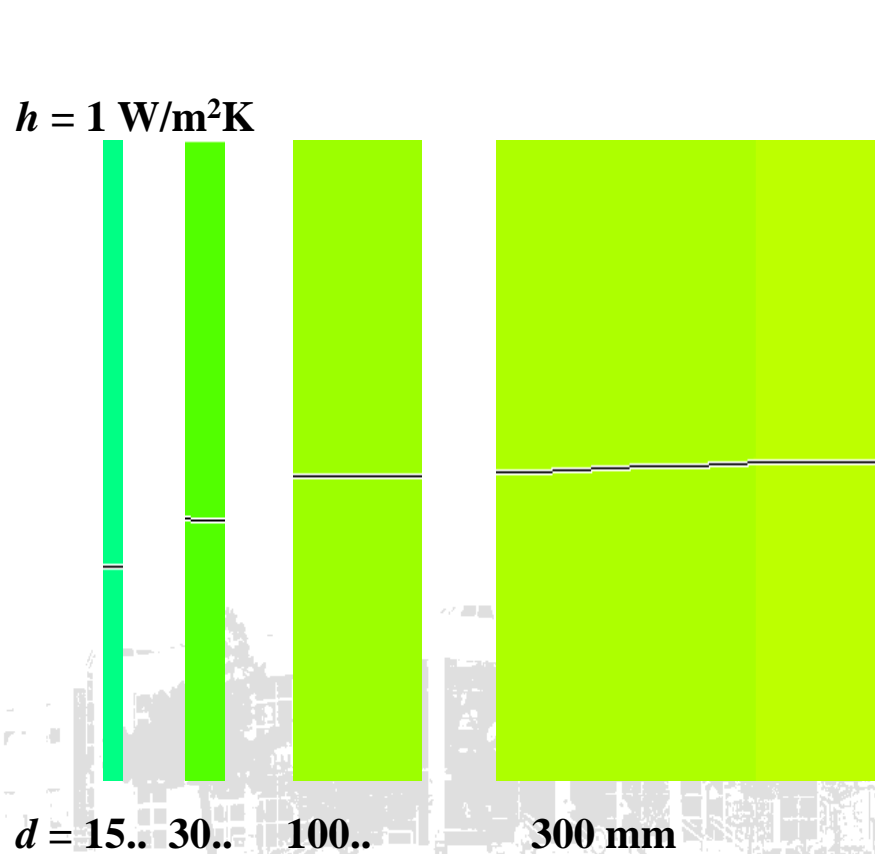
Slab thickness

- **Low heat transfer coefficient:**
No increase in heat storage capacity for $d > 30$ mm
- **High heat transfer coefficient:**
Increase in heat storage capacity until a maximum
- **Optimum thickness depending on heat transfer coefficient**
 - $h = 5 \text{ W/m}^2\text{K}$: $d_{opt} = 90\text{mm}$
 - $h = 30 \text{ W/m}^2\text{K}$: $d_{opt} = 140\text{mm}$



Diurnal heat storage capacity, c_{dyn} of a concrete slab depending on the thickness, d for different heat transfer coefficients, h .

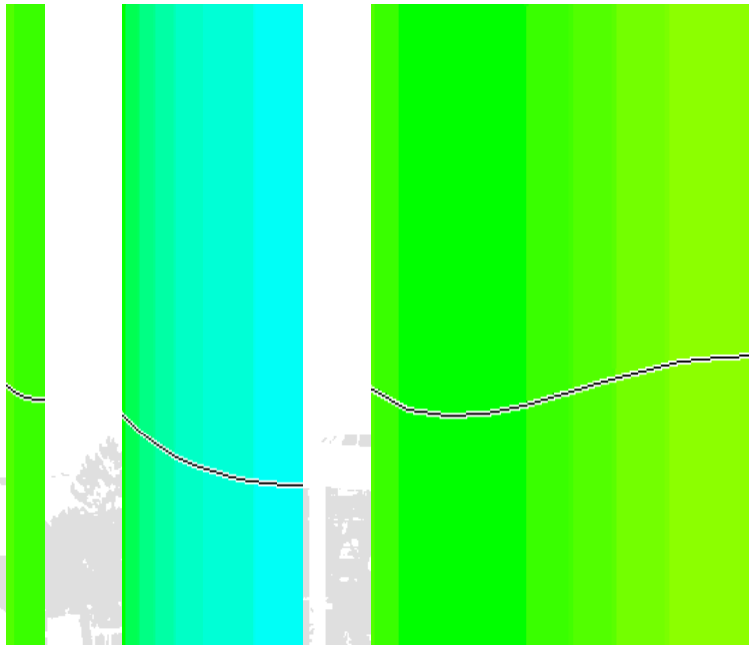
Slab thickness



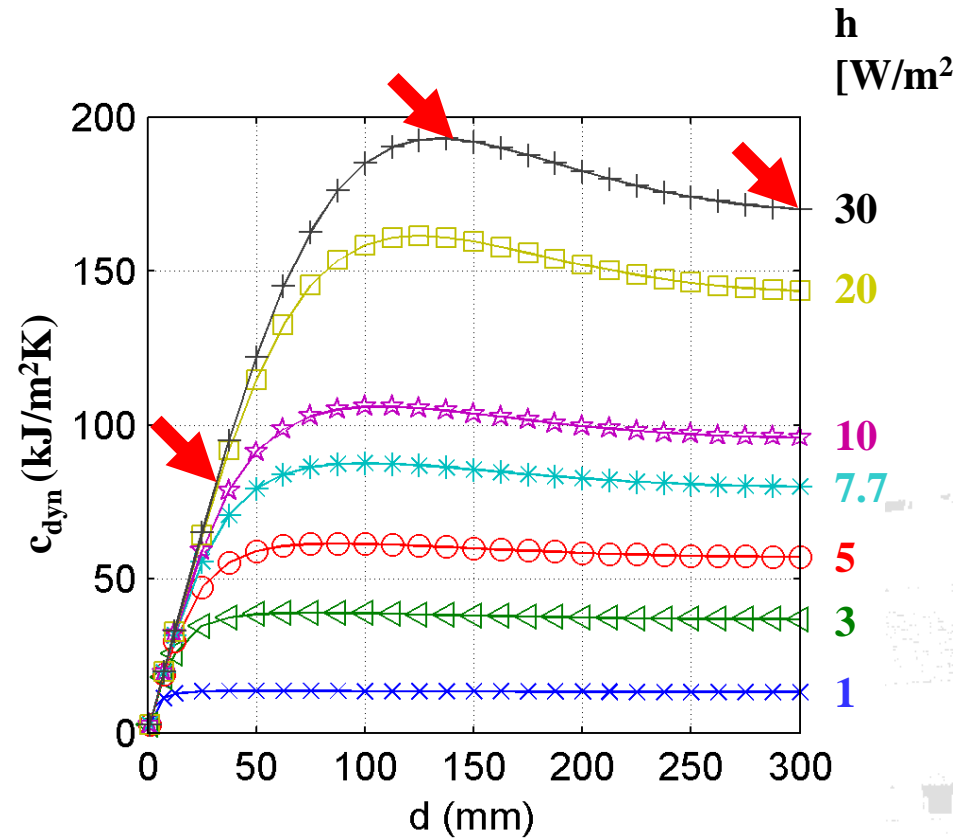
Diurnal heat storage capacity, c_{dyn} of a concrete slab depending on the thickness, d for different heat transfer coefficients, h .

Slab thickness

$h = 30 \text{ W/m}^2\text{K}$



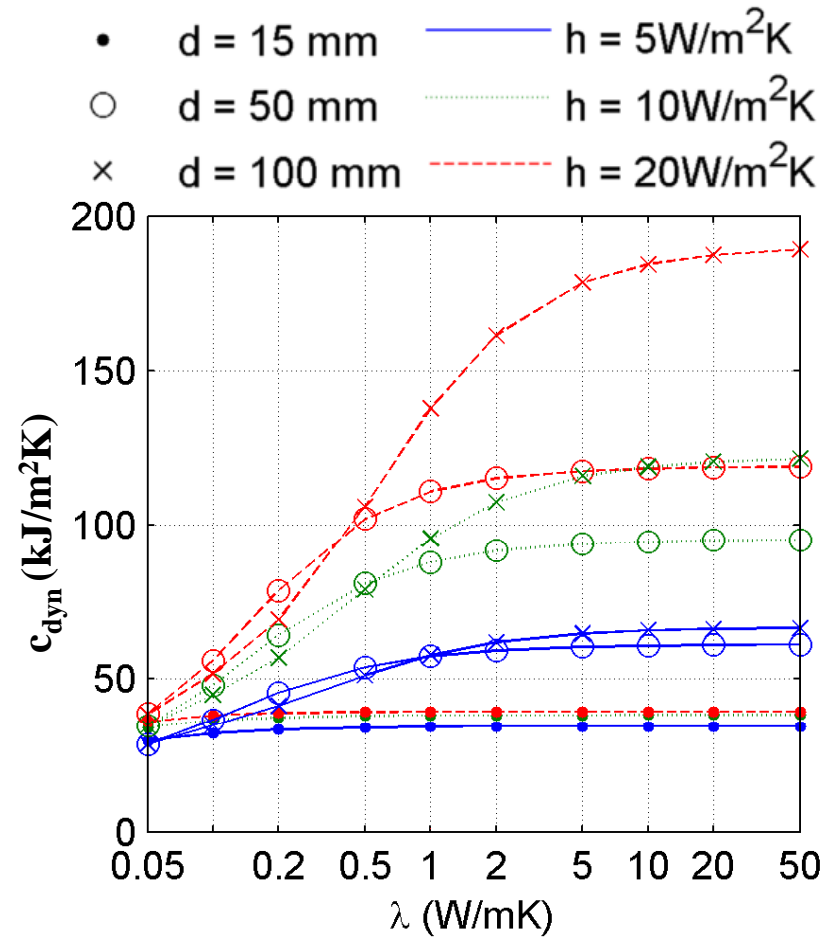
$d = 30..$ $140..$ 300 mm



Diurnal heat storage capacity, c_{dyn} of a concrete slab depending on the thickness, d for different heat transfer coefficients, h .

Thermal conductivity

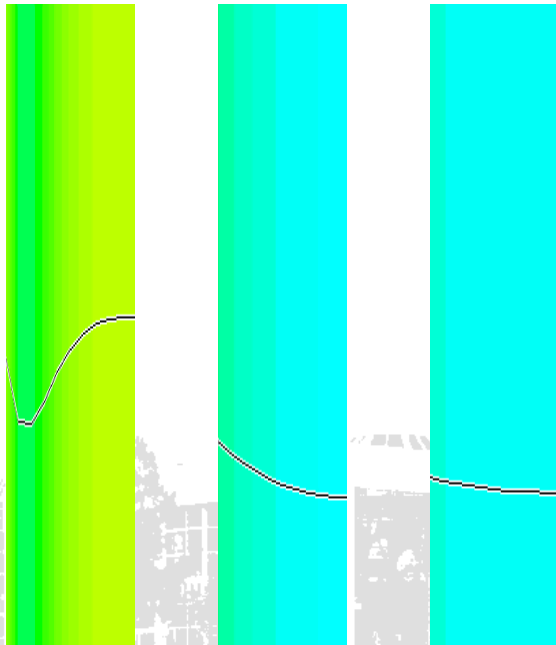
- Thin slab ($d = 15$ mm):
No impact of the thermal conductivity, λ
- Thick slabs:
Increase in heat storage capacity up to $\lambda \approx 1.8$ W/mK
- Above $\lambda = 1.8$ W/mK:
Further increase only for thick slabs ($d = 100$ mm) and high HTC ($h = 20$ W/m²K)



Diurnal heat storage capacity, q depending on the thermal conductivity, λ for different heat transfer coefficients, h and slab thicknesses, d ; $\rho c = 2.6$ MJ/m³K.

Thermal conductivity

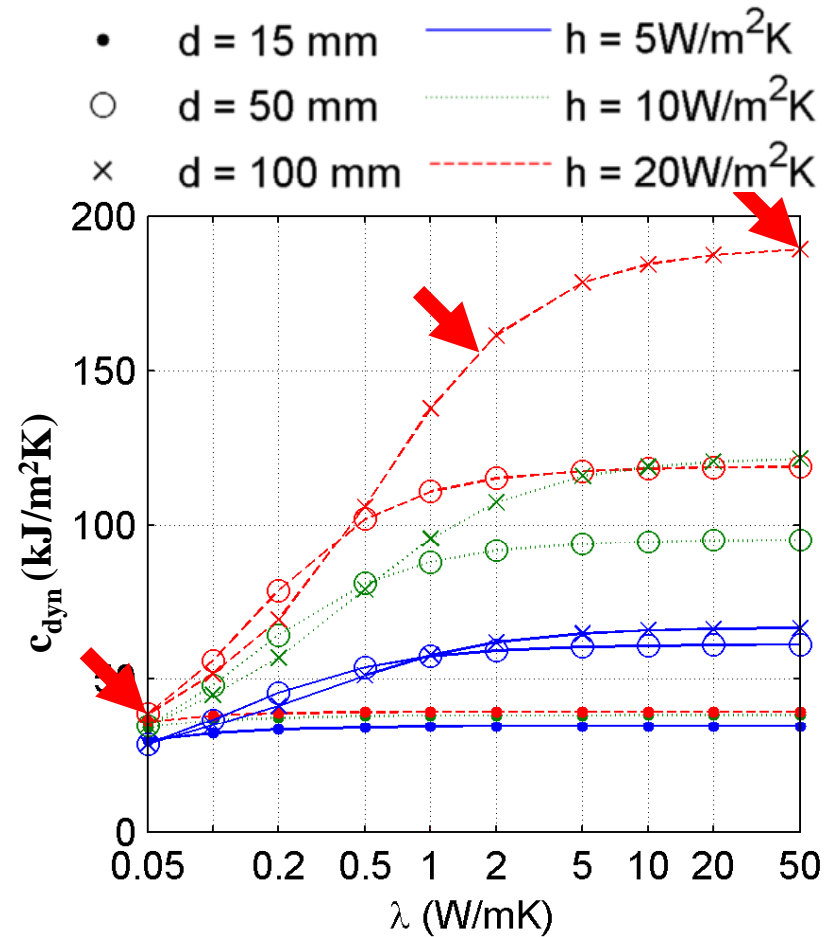
$d = 100 \text{ mm}; h = 20 \text{ W/m}^2\text{K}$



$\lambda = 0.05..$

$1.8..$

50 W/mK



Diurnal heat storage capacity, c_{dyn} depending on the thermal conductivity, λ for different heat transfer coefficients, h and slab thicknesses, d ; $\rho c = 2.6 \text{ MJ/m}^3\text{K}$.

Conclusions

Dynamic heat storage capacity can be limited by...

... the total thermal capacity of the element (d , ρc)

→ Typically not problematic for concrete elements

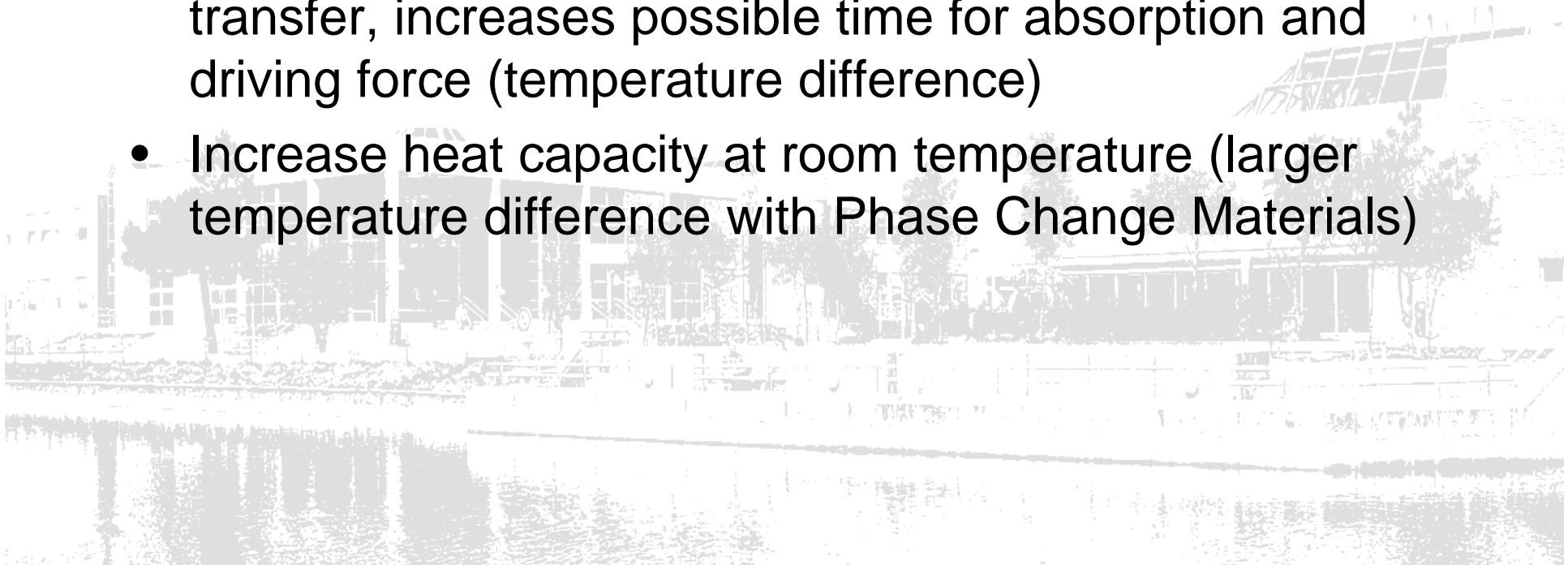
... the heat transfer (h , λ)

→ In most cases the thermal conductivity of concrete ($\lambda = 1.8 \text{ W/mK}$) is sufficient

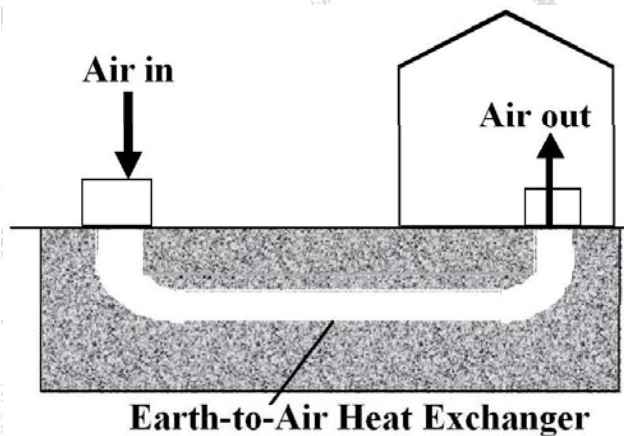
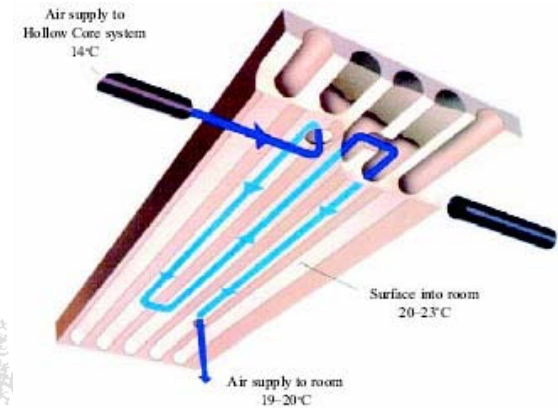
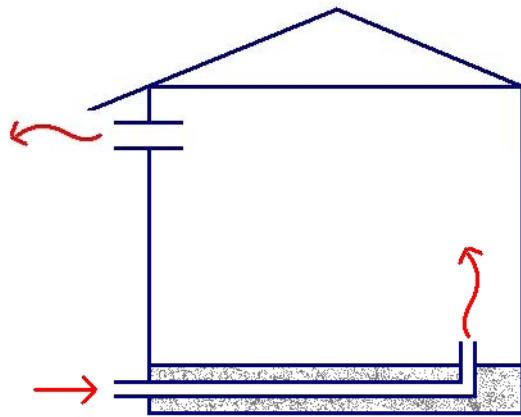
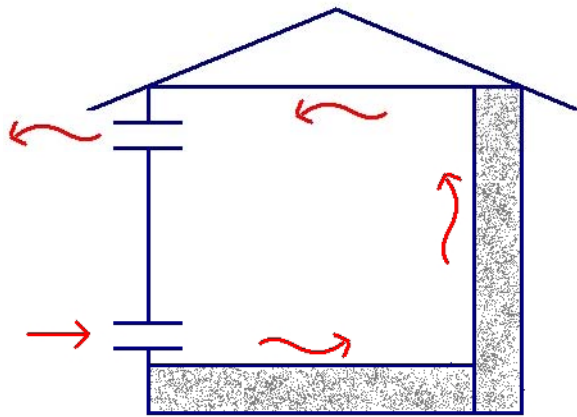
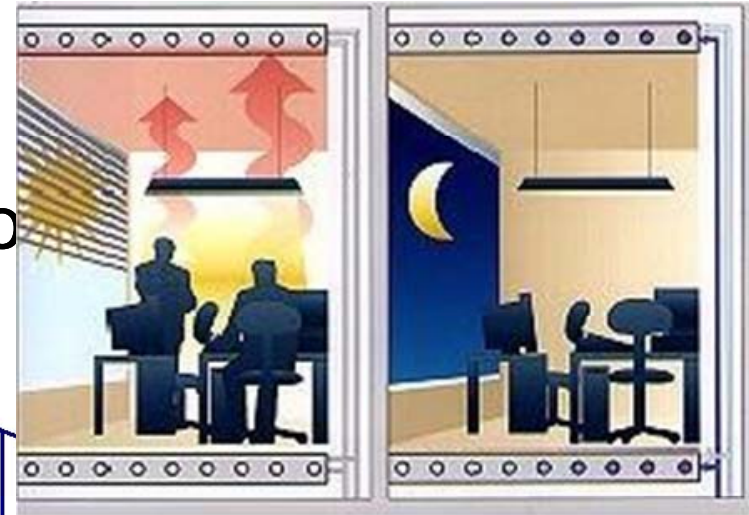
→ The most typical limiting factor is the surface heat transfer

Solutions

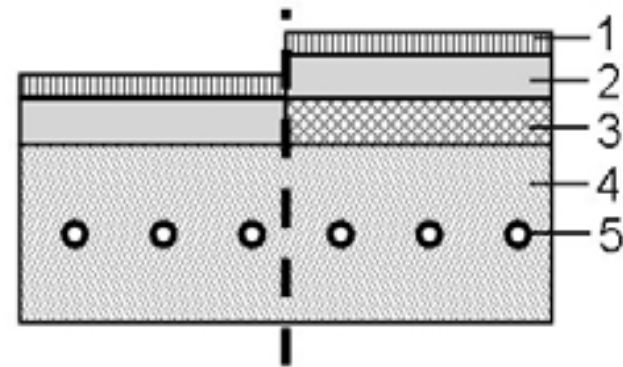
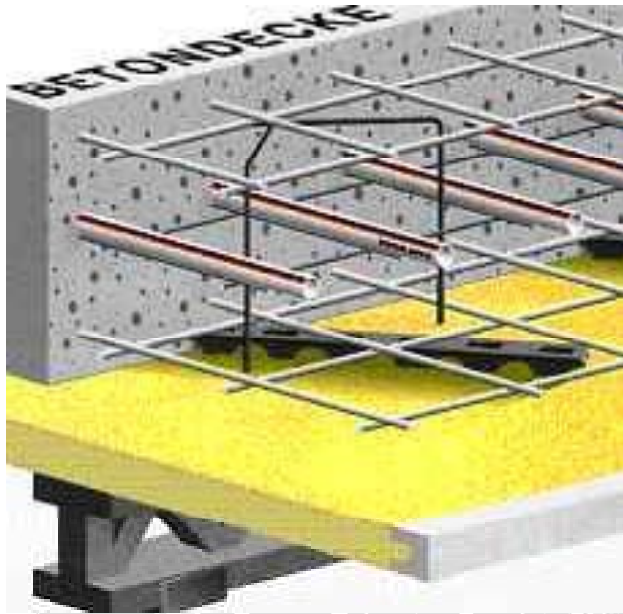
- Ensure large radiation exchange (solar radiation, cool surfaces in the view)
- Increase surface area
- Extract heat from construction core (one – way heat transfer, increases possible time for absorption and driving force (temperature difference))
- Increase heat capacity at room temperature (larger temperature difference with Phase Change Materials)



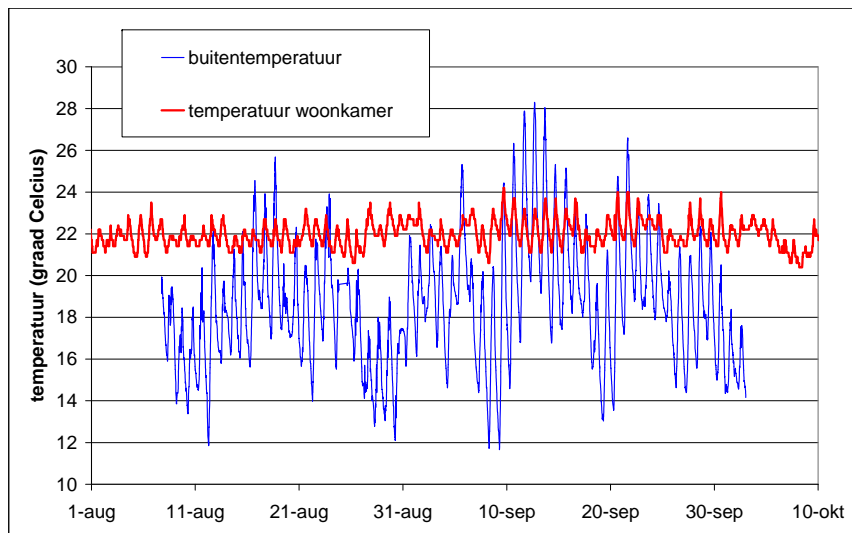
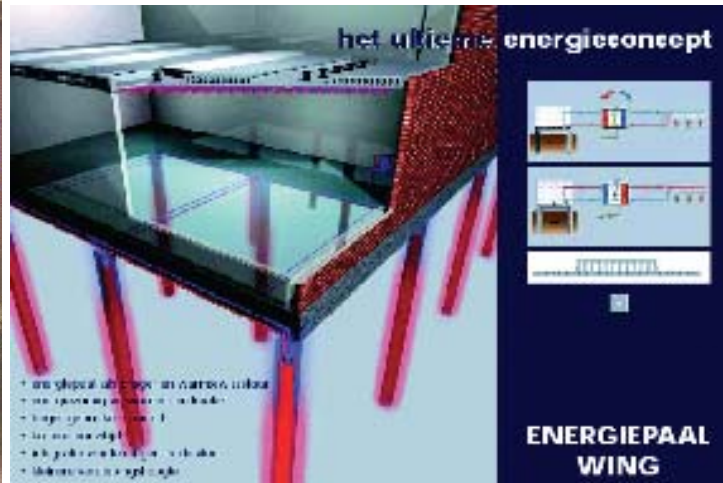
Examples of Air Based Solution



Water based system

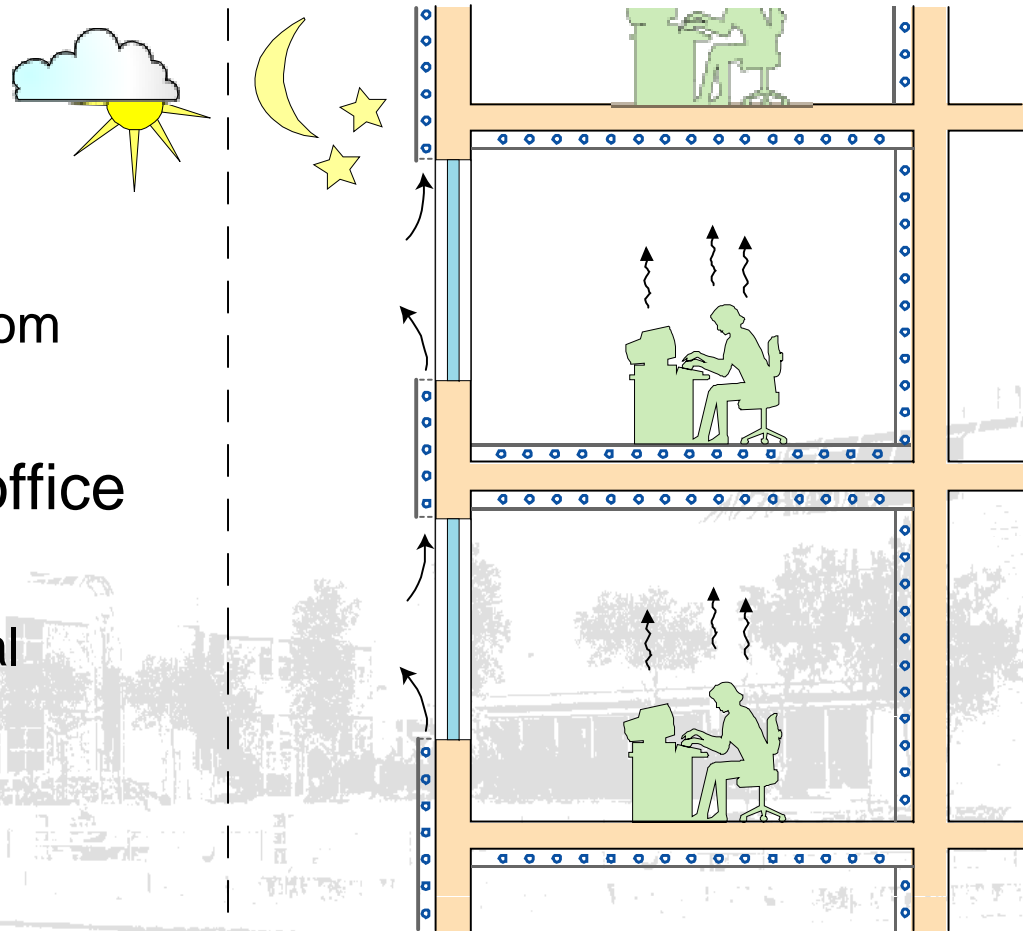


Energy piles with CCC



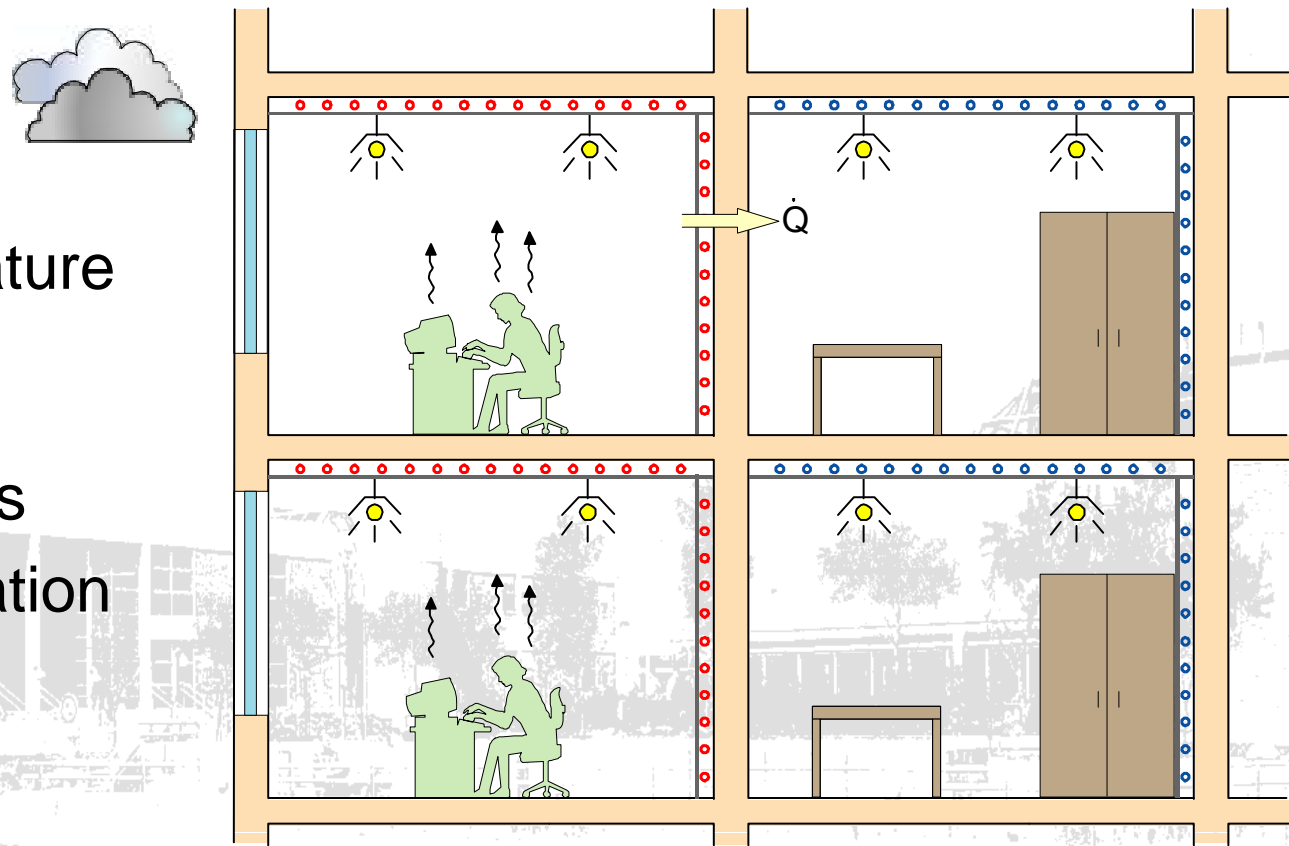
Energy Transfer from Rooms to the Façade

- Using temperature differences
 - between façade and room
 - between night and day
- Increased cooling for office building
 - combination with natural ventilation
 - high comfort standard



Energy Transfer between Rooms

- Using temperature and load differences between rooms
- Thermal activation of building basements



Conclusion

- Activation of thermal mass can make a difference
- Significant climatic cooling potential by night-time ventilation for most locations in Northern, Central and Eastern Europe
- The dynamic heat storage capacity of concrete can be increased by:
 - Focusing on radiation exchange of heat
 - Increasing surface area
 - Extract heat from construction core
 - Increase heat capacity at room temperature by phase change materials

